



Application of Analytical Element Model to Bioventing

Andrew Kirkman - bp
M Del Ciello – Sovereign Consulting
Jorge Montoy – Sovereign Consulting
Alex McCormick – Sovereign Consulting
bp RM Digital Team

P&O - remediation management
production & operations

Today's Discussion



Site Description



Discuss basis for estimating biodegradation rates for bioventing or aerobic respiration



Introduce Analytical Element Approach Applied to Bioventing



Provide Results & Discussion

Site Setting

Former Refinery overlying a sand aquifer

Aquifer is heavily influenced by

- Seasonal fluctuations in adjacent river resulting in groundwater flow direction reversals with various river stages
- Local industrial groundwater extraction

Historic LNAPL recovery and natural processes result in remaining impacts dominated by immobile residual LNAPL, a source of dissolved phase impacts

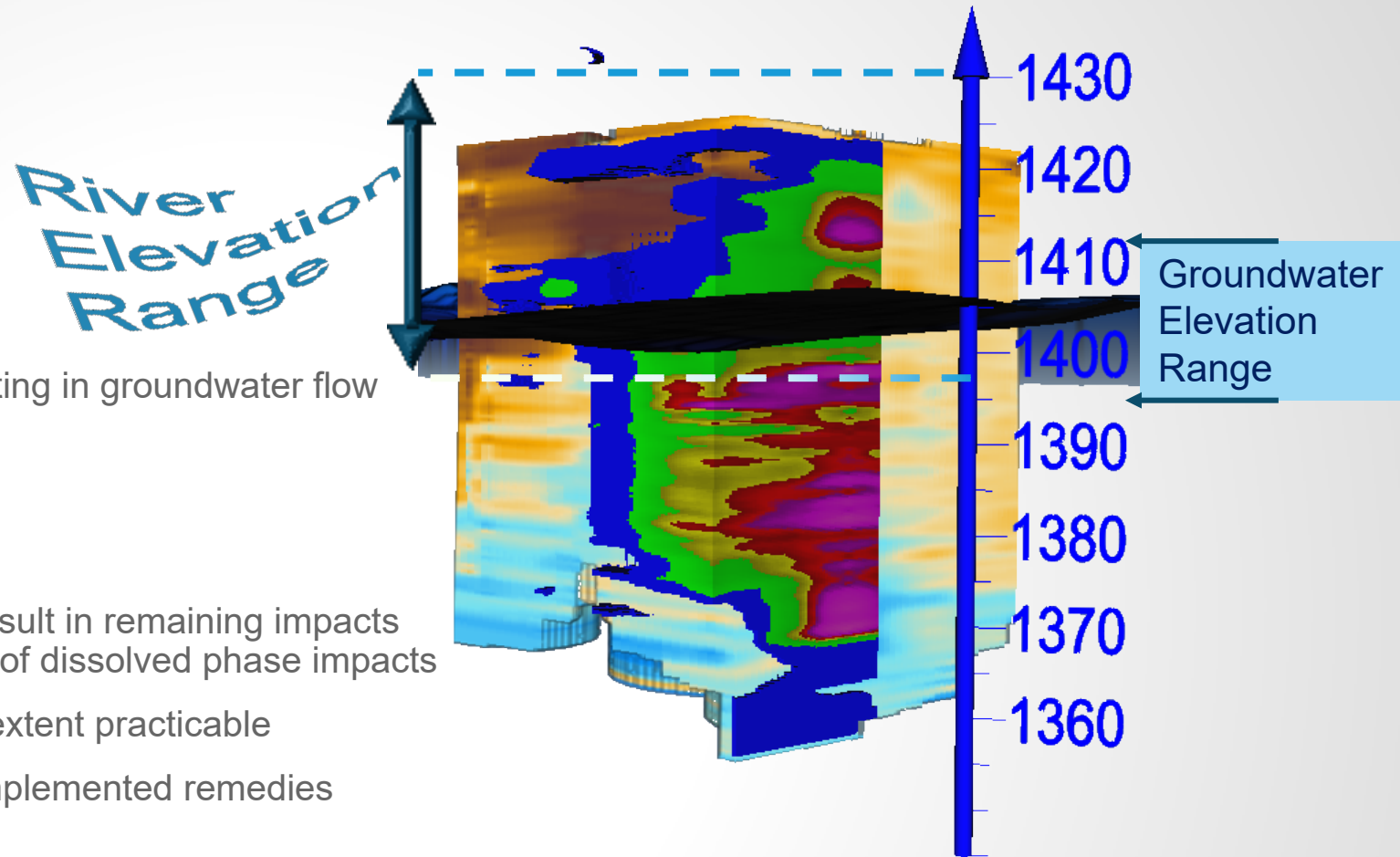
Regulatory framework does not define maximum extent practicable

Work to define remedial transition/endpoints for implemented remedies acceptable to all stakeholders

Site Approach (Simplified)

LNAPL Recovery will be performed for LNAPL transmissivity values $>2 \text{ ft}^2/\text{day}$ as measured at seasonal low water-table

Enhance biodegradation to progress dissolved phase remedial objective and represent alternative to the historical perspective of recovery to zero thickness



Standard Respiration Testing

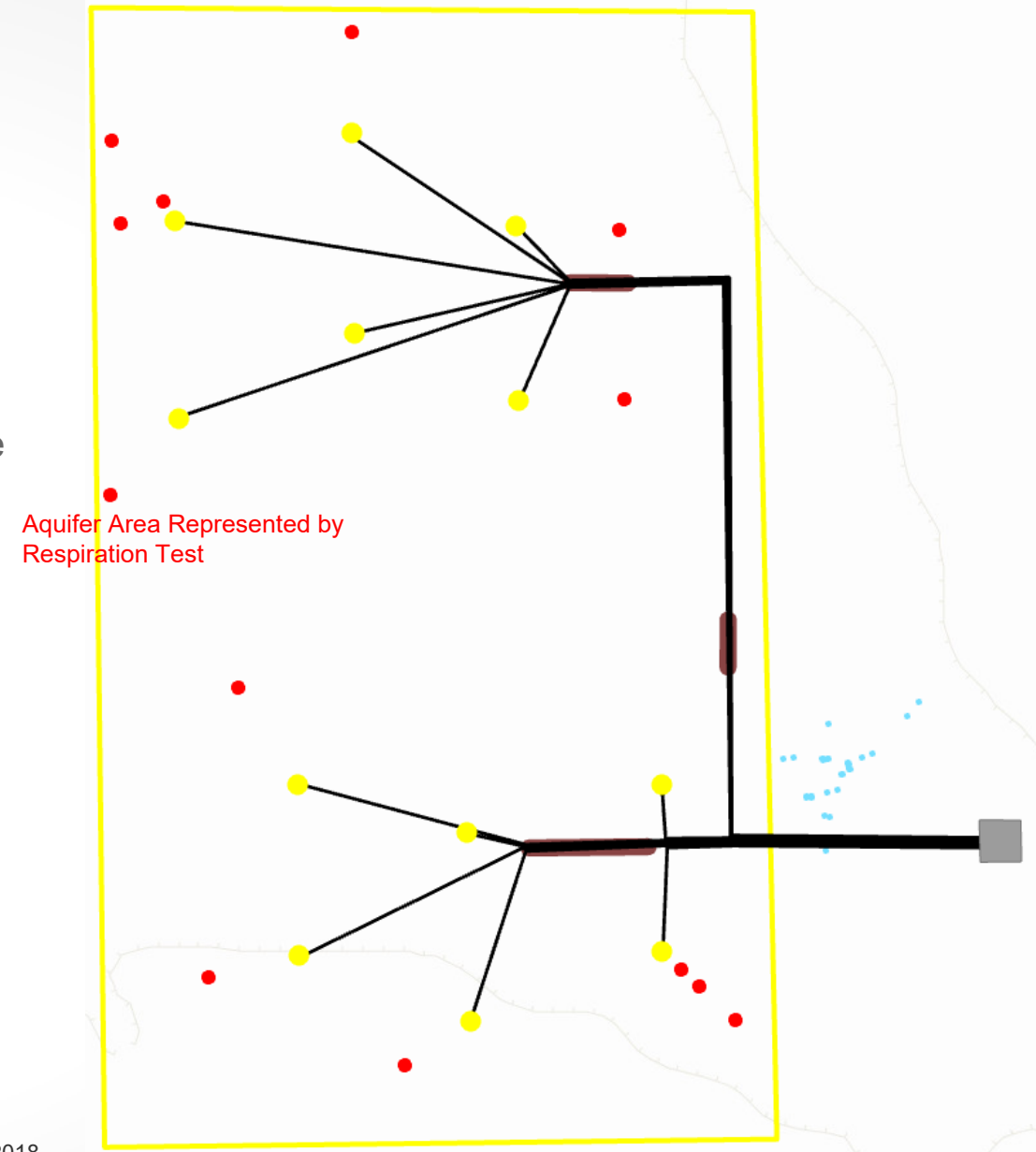
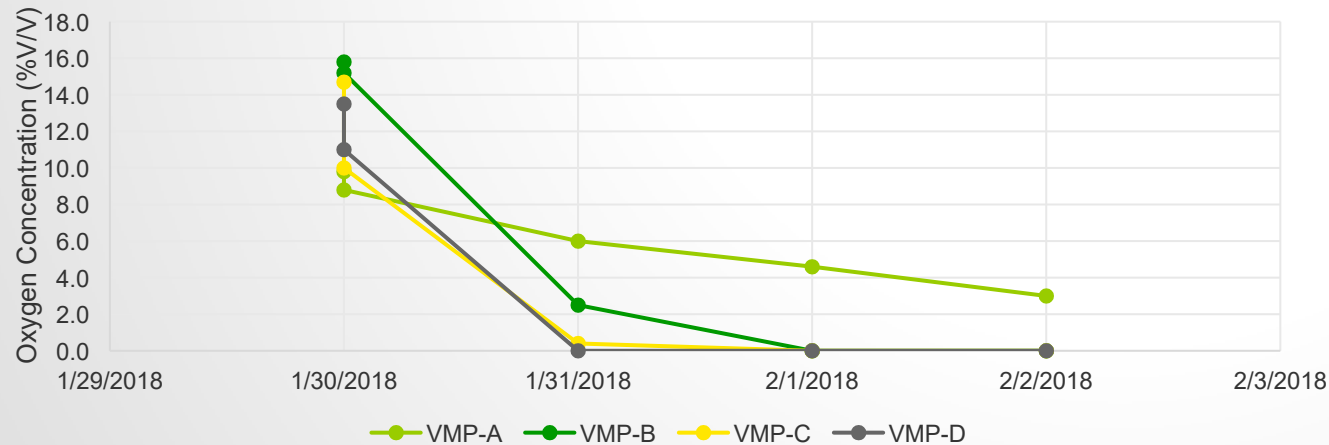
Run System → then Shutoff after a sufficient operation period

Measure change in oxygen over time at a given vapor monitoring point

Select appropriate trend and fit a line to oxygen over time

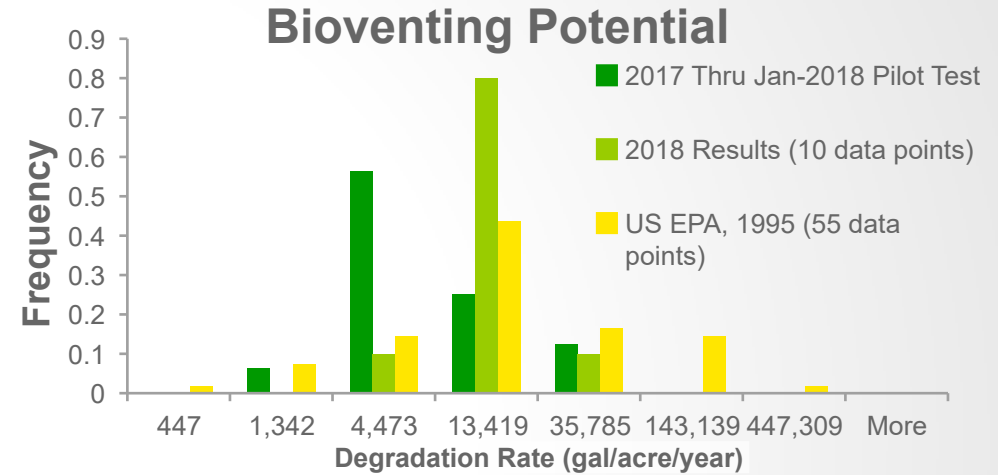
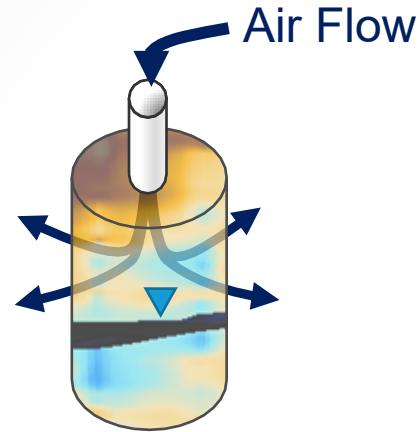
- Data needs to be filtered for time, soil gas values that result in the ~maximum rate of O₂ utilization linear behavior
- Linear behavior often does not occur at start or end of the test
- Coding data point selection for trend analysis is challenging
- Linear trends are fit manually

Example Respiration Test Data

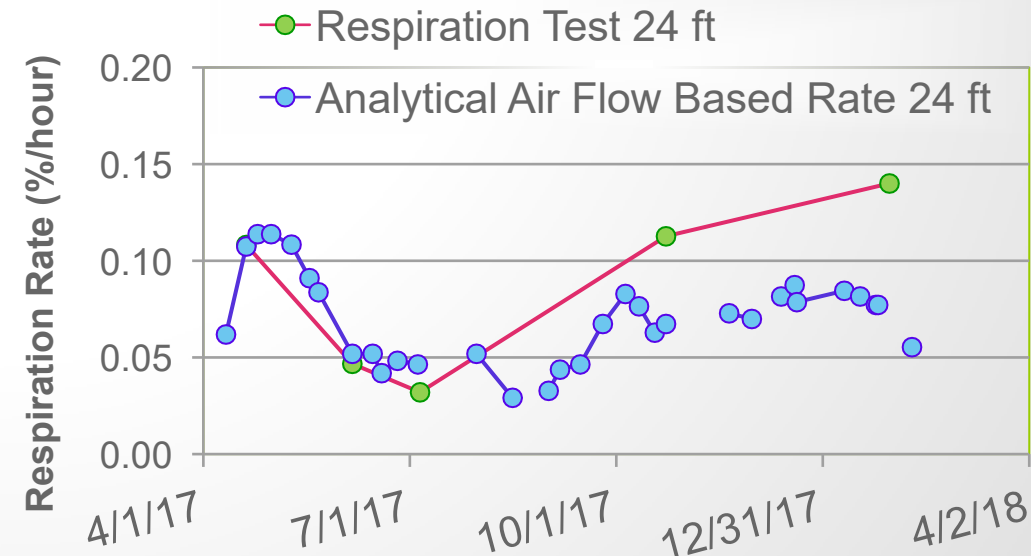


Analytical Approach

Radial Flow Solution in a Confined Vadose Zone



Note: US EPA Results multiplied by equivalent depth to pilot site for comparison purposes



Benefits

- Continuous measurement during operation
- Reduces Diffusion Effects?
- Can minimize effects from water-table fluctuations

Gaps

- Susceptible to permeability heterogeneity?

Multiple Wells Is More Complex

Goals of an Analytical Element Method (AEM)

- Estimate rates during operation
- Optimize data management/Analysis
- Optimization decisions based on monthly trends data rather than biannual events

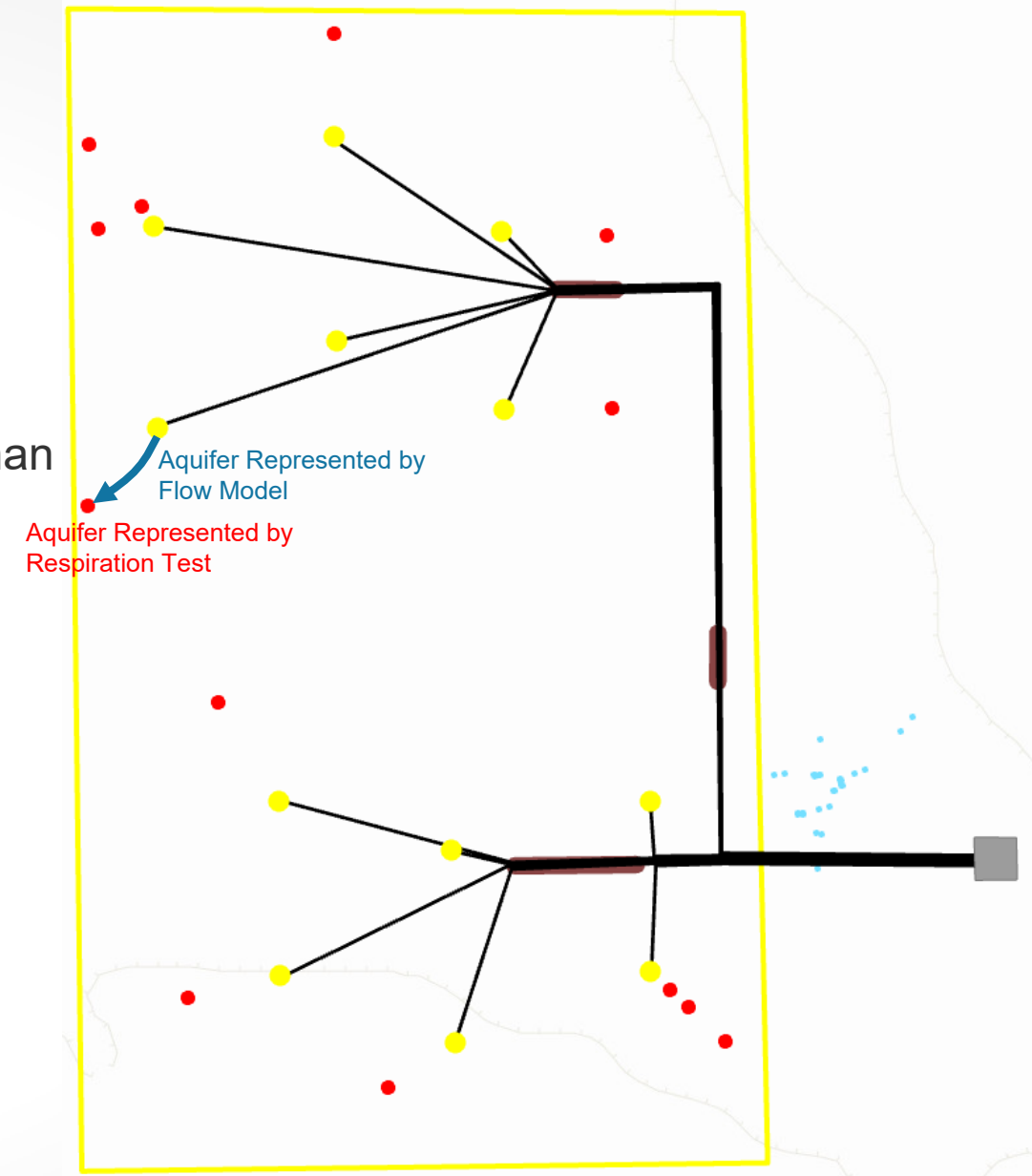
Able to account for water-table fluctuations

Leveraged Analytical Element Method (Strack, 1989)

- Can be incorporated into Python Scripts and Automated Dashboards
- Steady State Representation
 - Calculated rates following a system startup do not reflect actual biodegradation rates
 - Treatment Area is ~400 X 700 ft
 - Would require minimum of 200 hours of operation to replace the soil gas volume

Considered MS-DOS and Mod-flow based Air3D (USEPA)

VMP's were located with this application in mind



Analytical Element Method

(AEM) after Strack, 1989

Goal: Calculate the time it takes air to travel to a given vapor point

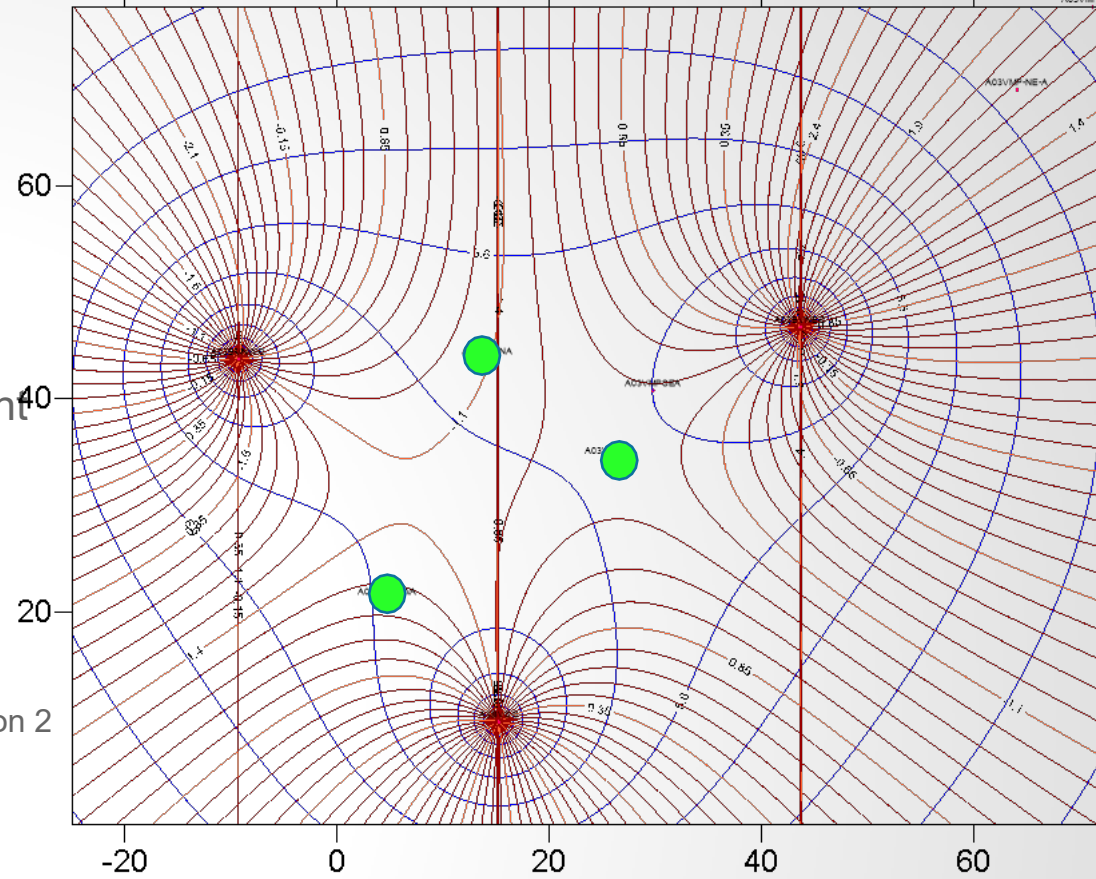
1. Calculate Stream Function (ψ) at the desired vapor monitoring point

Air Flow Head Potential

Equation 1

Equation 2

Stream Lines

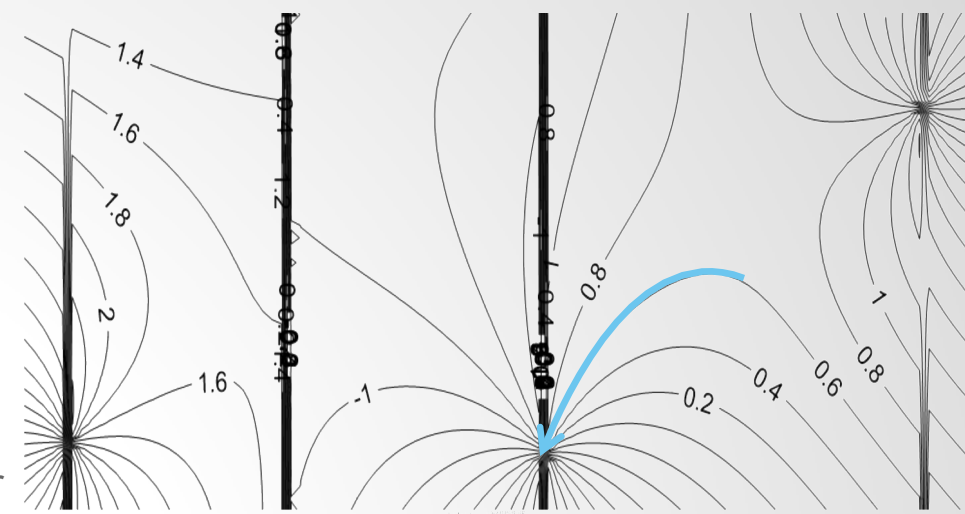


$$\psi = \frac{Q_1}{2\pi} \arctan\left(\frac{y-y_1}{x-x_1}\right) + \frac{Q_2}{2\pi} \arctan\left(\frac{y-y_2}{x-x_2}\right) + \dots + \frac{Q_n}{2\pi} \arctan\left(\frac{y-y_n}{x-x_n}\right)$$

AEM Process (continued)

2. Find Distance Back to original Biovent well

1. Use Complex Coordinates for discharge vectors in x & y direction
2. Forecast next point based on current location z plus the discharge vector
3. Iterate using Newton-Rhapson Method to resolve z to the desired precision
4. Log the distances along the generated path of points



$$\bar{W} = Q_x + Q_y i$$



$$Q_x = -\frac{\delta\psi}{\delta y}$$

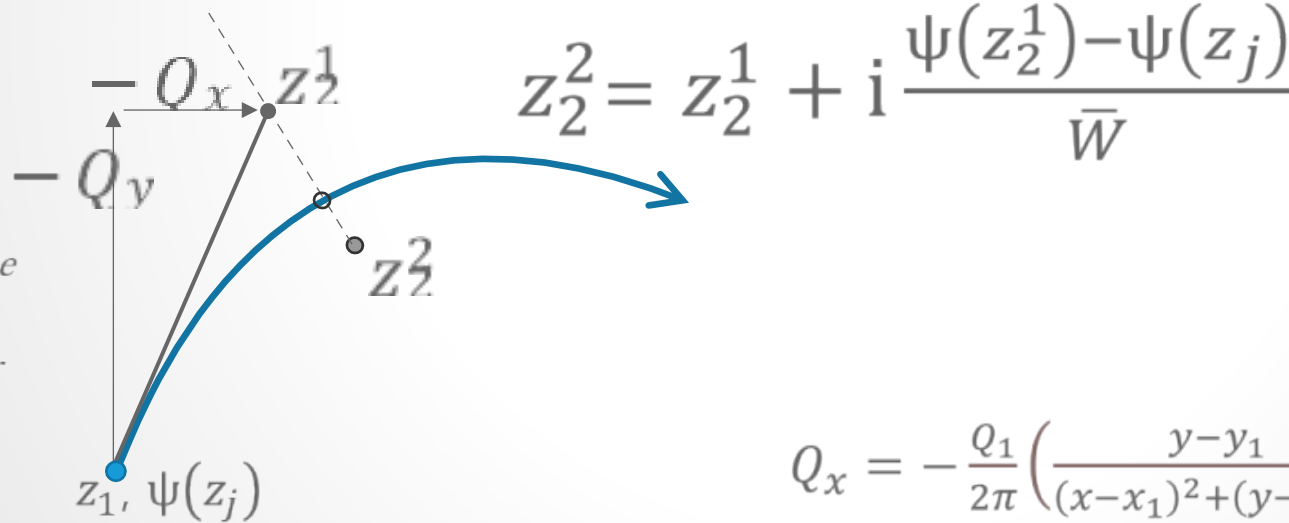
$$Q_y = \frac{\delta\psi}{\delta x}$$



Differentiating Equation 3

$$Q_x = -\frac{Q_1}{2\pi} \left(\frac{y-y_1}{(x-x_1)^2+(y-y_1)^2} \right) - \dots - \frac{Q_n}{2\pi} \left(\frac{y-y_n}{(x-x_n)^2+(y-y_n)^2} \right)$$

$$Q_y = \frac{Q_1}{2\pi} \left(\frac{x-x_1}{(x-x_1)^2+(y-y_1)^2} \right) - \dots - \frac{Q_n}{2\pi} \left(\frac{x-x_n}{(x-x_n)^2+(y-y_n)^2} \right)$$



Complex Coordinate Plane

$$\bar{z} = x + yi$$

\bar{W} - discharge vector

AEM Process (continued)

Travel time (t) for a given distance (d) segment is calculated using seepage velocity

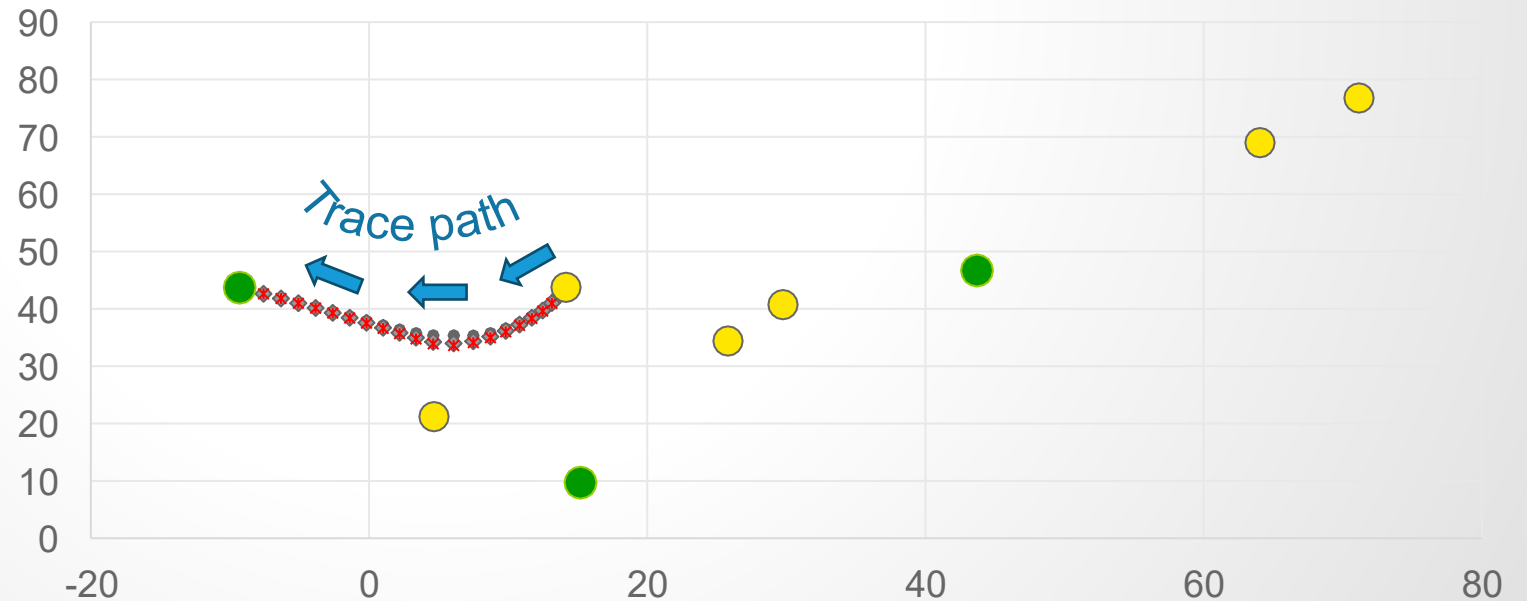
Linear head difference used to approximate gradient

$$t = \frac{d}{v} \cong \frac{d}{\frac{k}{n} \frac{\phi_{Z_2} - \phi_{Z_1}}{d}} = \frac{d^2 n}{k(\phi_{Z_2} - \phi_{Z_1})} = \frac{d^2 n}{\frac{Q_1}{2\pi H} \ln\left(\frac{r_{BV1_Z_2}}{r_{BV1_Z_1}}\right) + \dots + \frac{Q_i}{2\pi H} \ln\left(\frac{r_{BVi_Z_2}}{r_{BVi_Z_1}}\right)}$$

After Equation 2

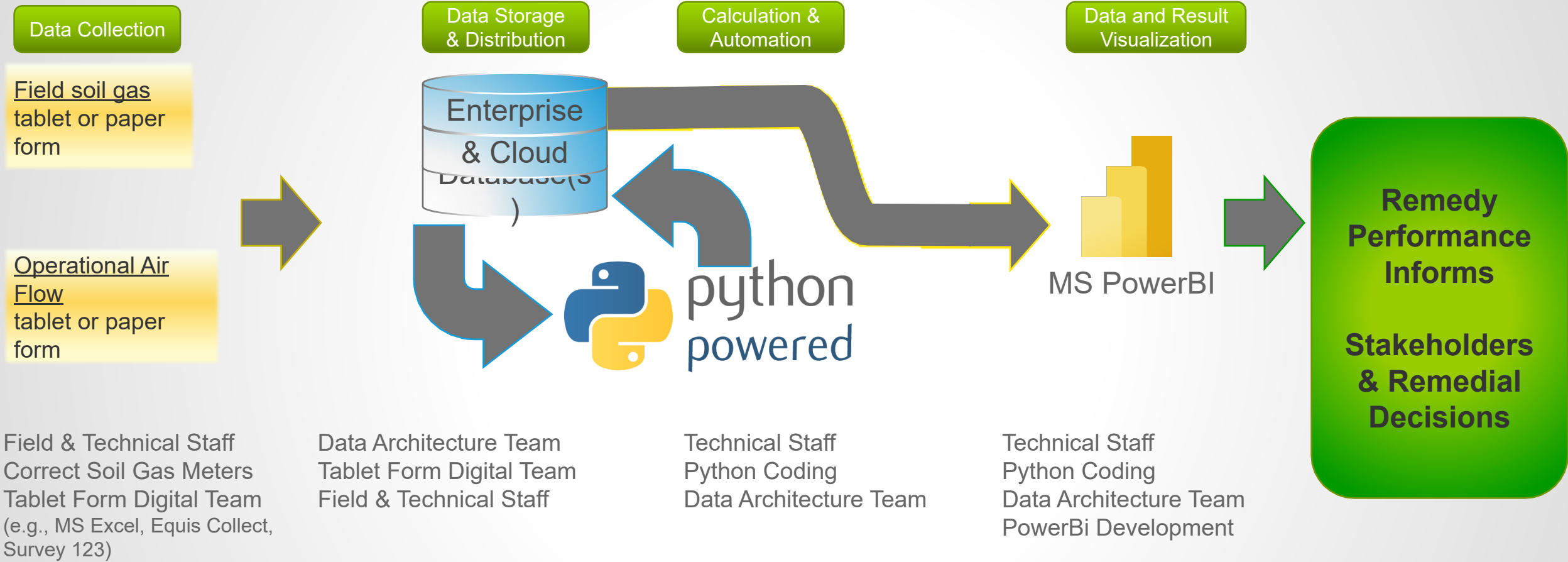
- Run 1
- ◆ Run 2
- * Run 3
- VMP
- BV

Quick convergence for 3 Iterations



t – time
 d – distance
 n – porosity

Data Flow



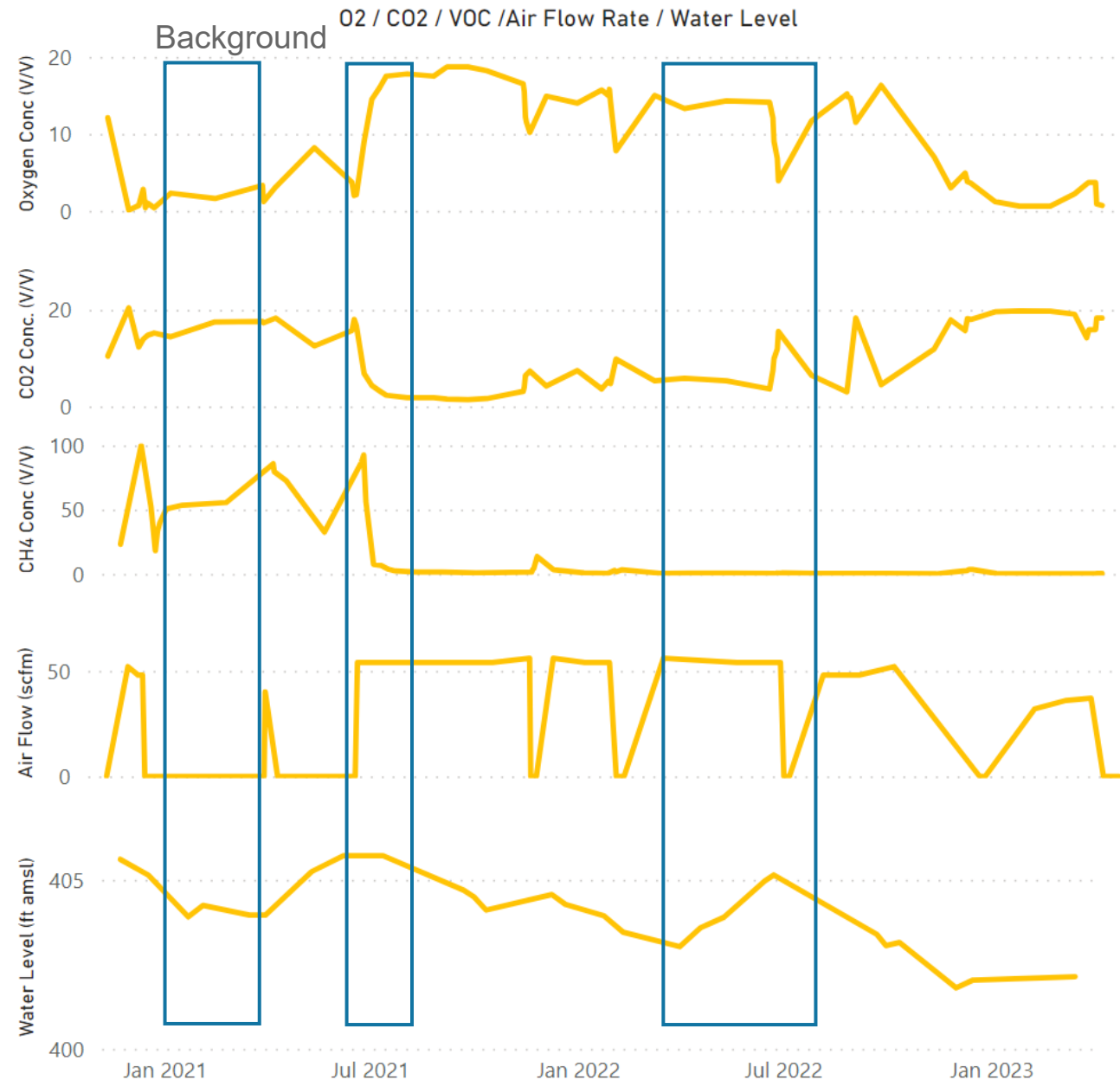
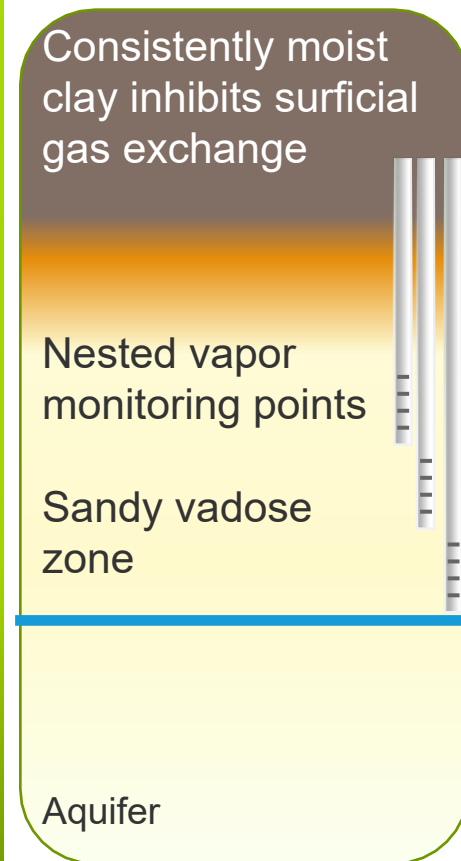
Digital Security

Soil Gas Behavior

Prior to continuous operation river induced oxygen concentration less than 2 percent

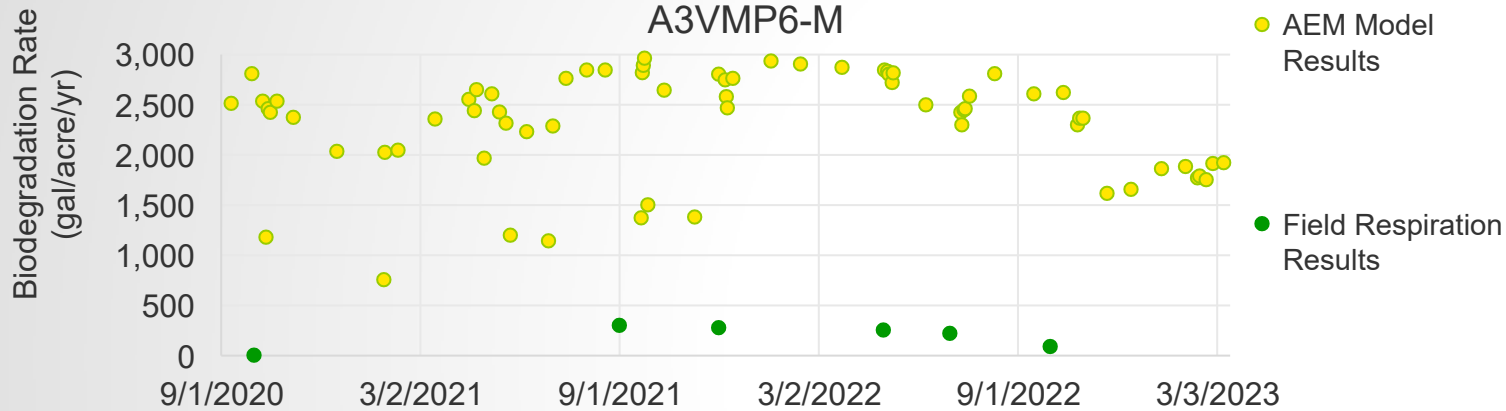
Operation of bioventing system increases oxygen concentrations above background

Groundwater elevation Induced flow not accounted for in model

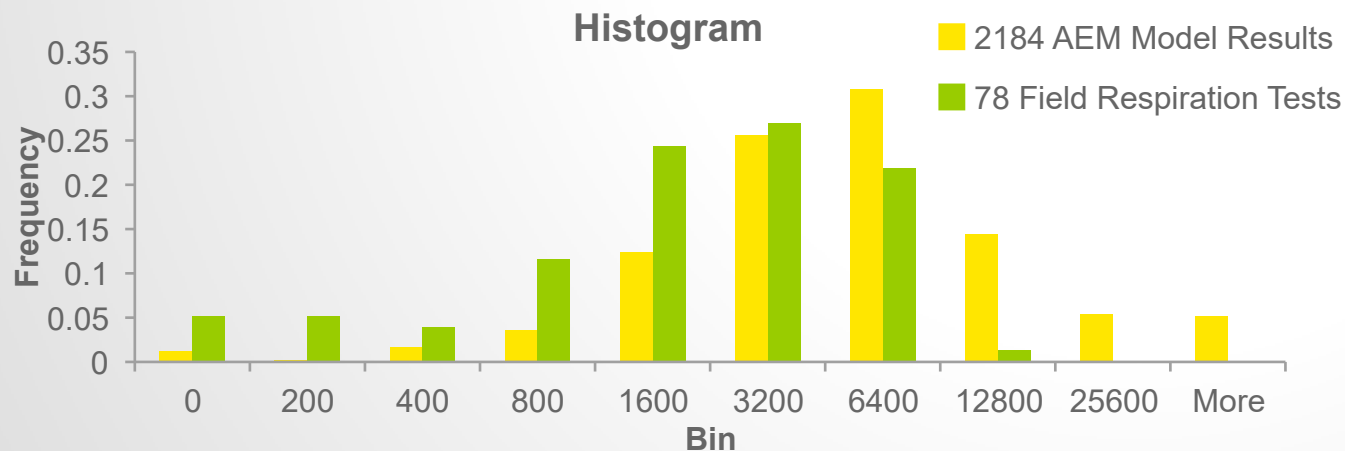


Comparison of Flow Model to Traditional Respiration Tests

- Results do not compare well at a singular location
- They do not represent the same spatial measure of space



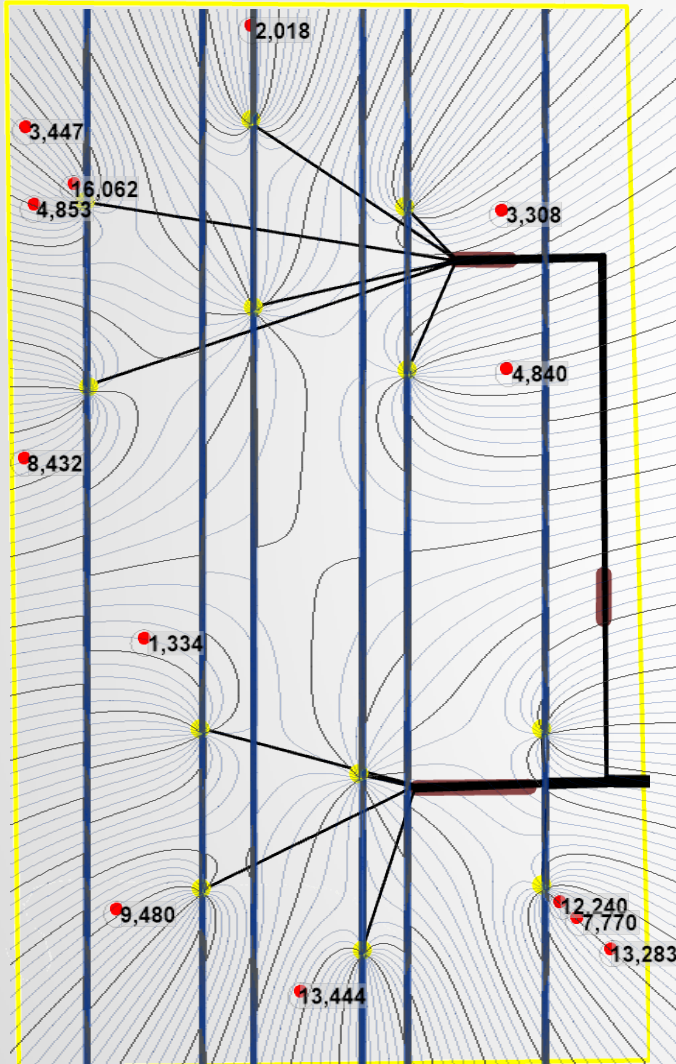
- Comparison of all locations may have room for optimism



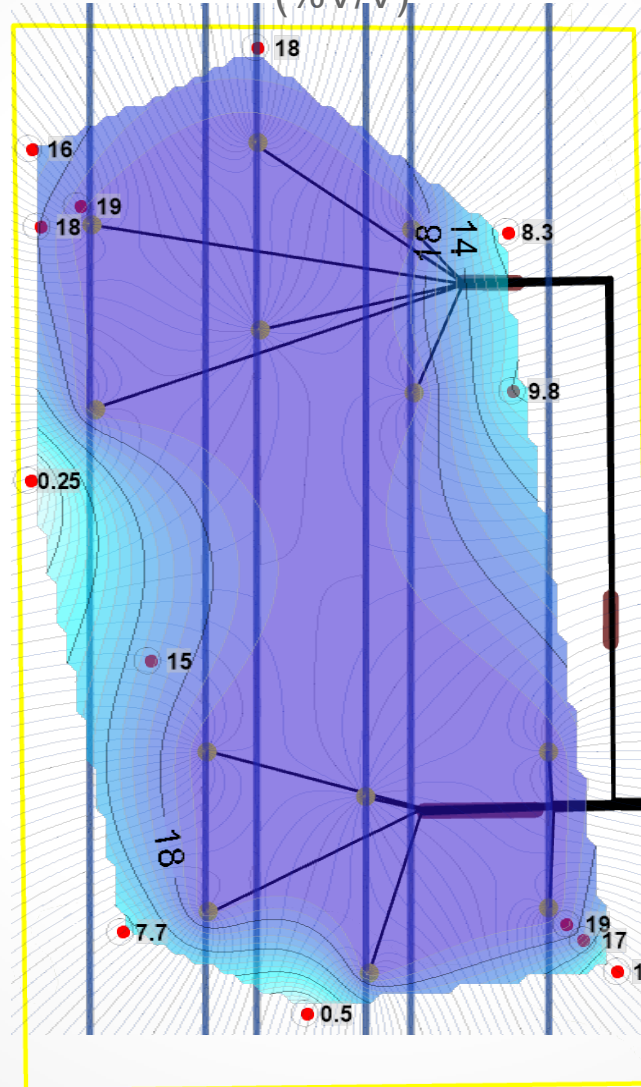
Monitoring Point (Depth)	Vertical Extent (feet)	October-20		September-21		December-21		May-22		July-22		October-22	
		gal-NAPL/acre/year		gal-NAPL/acre/year		gal-NAPL/acre/year		gal-NAPL/acre/year		gal-NAPL/acre/year		gal-NAPL/acre/year	
		gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year	gal-NAPL/acre/year
A3VMP1 (17)	5.00	2,939	5,061	609		700		310		477		1,689	
A3VMP1 (22)	5.00	2,122		732	1,341	816	1,516	1,066	4,000	404	881	1,733	5,216
A3VMP1 (27)	5.00	--		--		--		2,624		--		1,794	
A3VMP2 (17)	5.00	1,866	3,918	1,982		1,143		958		657		799	
A3VMP2 (22)	5.00	2,052		2,495	4,478	1,796	2,939	1,564	7,187	1,182	1,838	641	1,879
A3VMP2 (27)	5.00	--		--		--		4,664		--		440	
A3VMP3 (17)	5.00	233	233	1,563		1,283		1,263		461		437	
A3VMP3 (22)	5.00	0		1,026	2,589	1,259	2,542	1,223	2,486	450	911	242	922
A3VMP3 (27)	5.00	--		--		--		--		--		242	
A3VMP4 (17)	5.00	1,329	4,501	2,006		1,189		1,445		451		2,511	
A3VMP4 (22)	5.00	3,172		1,842	3,848	910	3,312	1,356	3,320	455	1,851	1,876	5,216
A3VMP4 (27)	5.00	--		--		1,213		519		945		829	
A3VMP5 (17)	5.00	1,796	4,618	3,522		980		1,403		2,408		1,565	
A3VMP5 (22)	5.00	2,822		2,775	6,297	1,936	3,452	307	3,030	832	3,970	782	3,370
A3VMP5 (27)	5.00	--		--		536		1,320		730		1,023	
A3VMP6 (17)	5.00	1,399	1,702	886		886		--		342		320	
A3VMP6 (22)	5.00	303		280	1,166	257	1,399	--	0	223	564	91	412
A3VMP6 (27)	5.00	--		--		257		--		--		0	
A3VMP7 (17)	5.00	513	1,959	886		420		56		316		69	
A3VMP7 (22)	5.00	1,446		676	1,563	630	1,049	201	420	165	481	424	1,210
A3VMP7 (27)	5.00	--		--		--		163		--		717	
A3VMP8 (17)	5.00	303	1,633	1,259		1,073		660		624		1,017	
A3VMP8 (22)	5.00	1,329		1,119	2,379	770	2,892	451	1,140	672	1,746	1,191	3,180
A3VMP8 (27)	5.00	--		--		1,049		29		450		972	
A3VMP9 (17)	5.00	210	1,772	1,073		840		480		997		0	
A3VMP9 (22)	5.00	1,563		1,189	2,262	816	2,635	1,152	2,524	416	1,878	0	0
A3VMP9 (27)	5.00	--		--		980		892		465		0	
A3VMP10 (17)	5.00	420	956	117		396		--		193		24	
A3VMP10 (22)	5.00	536		117	233	420	840	--	0	148	392	66	98
A3VMP10 (27)	5.00	--		--		23		--		51		8	
A3VMP11 (17)	5.00	1,842	3,662	2,006		956		206		546		335	
A3VMP11 (22)	5.00	1,819		2,449	4,454	1,003	1,959	75	474	556	1,101	225	811
A3VMP11 (27)	5.00	--		--		--		193		--		251	
A3VMP12 (17)	5.00	327	583	396		513		610		136		211	
A3VMP12 (22)	5.00	257		443	840	606	1,119	687	1,559	19	155	141	874
A3VMP12 (27)	5.00	--		--		--		263		--		521	
A3VMP13 (17)	5.00	163	443	320		280		--		101		0	
A3VMP13 (22)	5.00	280		389	709	350	630	--	0	66	167	0	36
A3VMP13 (27)	5.00	--		--		--		--		--		36	
		2,388		2,474		2,022		2,011		1,226		1,786	
		AVERAGE TOTAL		AVERAGE TOTAL		AVERAGE TOTAL		AVERAGE TOTAL		AVERAGE TOTAL		AVERAGE TOTAL	

Degradation, Travel Time and Oxygen Concentrations

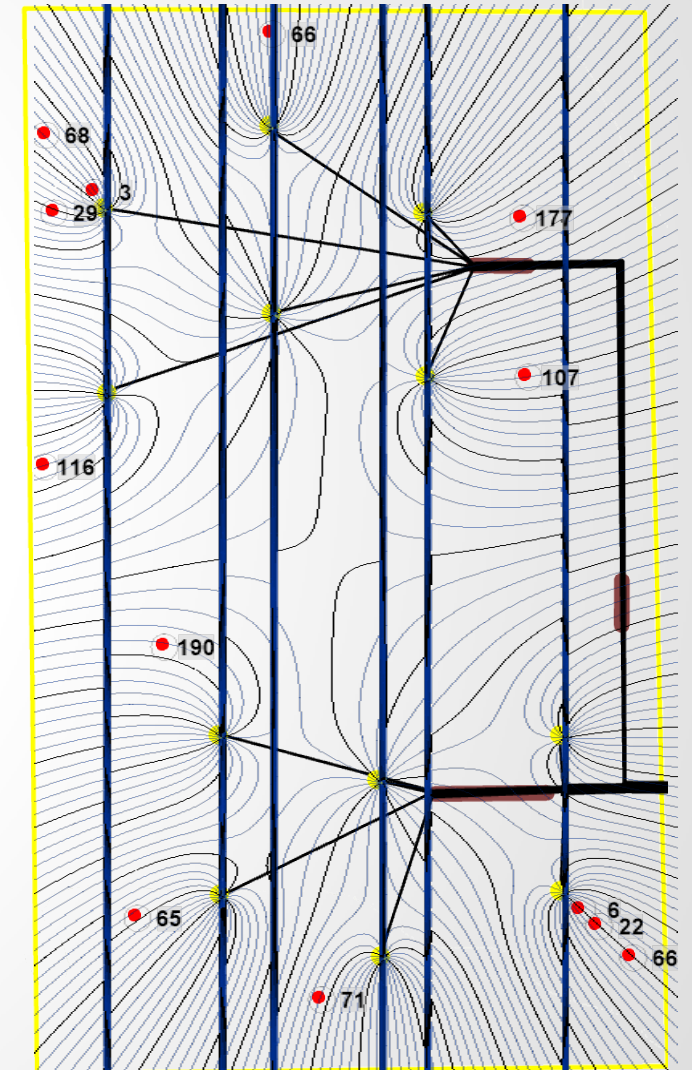
Biodegradation Rate
(gal/acre/yr)



Oxygen Concentration
(%V/V)



Travel Time



Comparison of Biodegradation Rates Needs to Consider What each Measure Represents

Respiration Field Tests – point Measure

- 14 points 2-3 depths and 6 events provide a reasonable space time average
- **Average Degradation across the design 6 acres → 12k gal/yr**

AEM Results represent the oxygen depletion that occurs from the biovent well out to the vapor monitoring point along a particle path

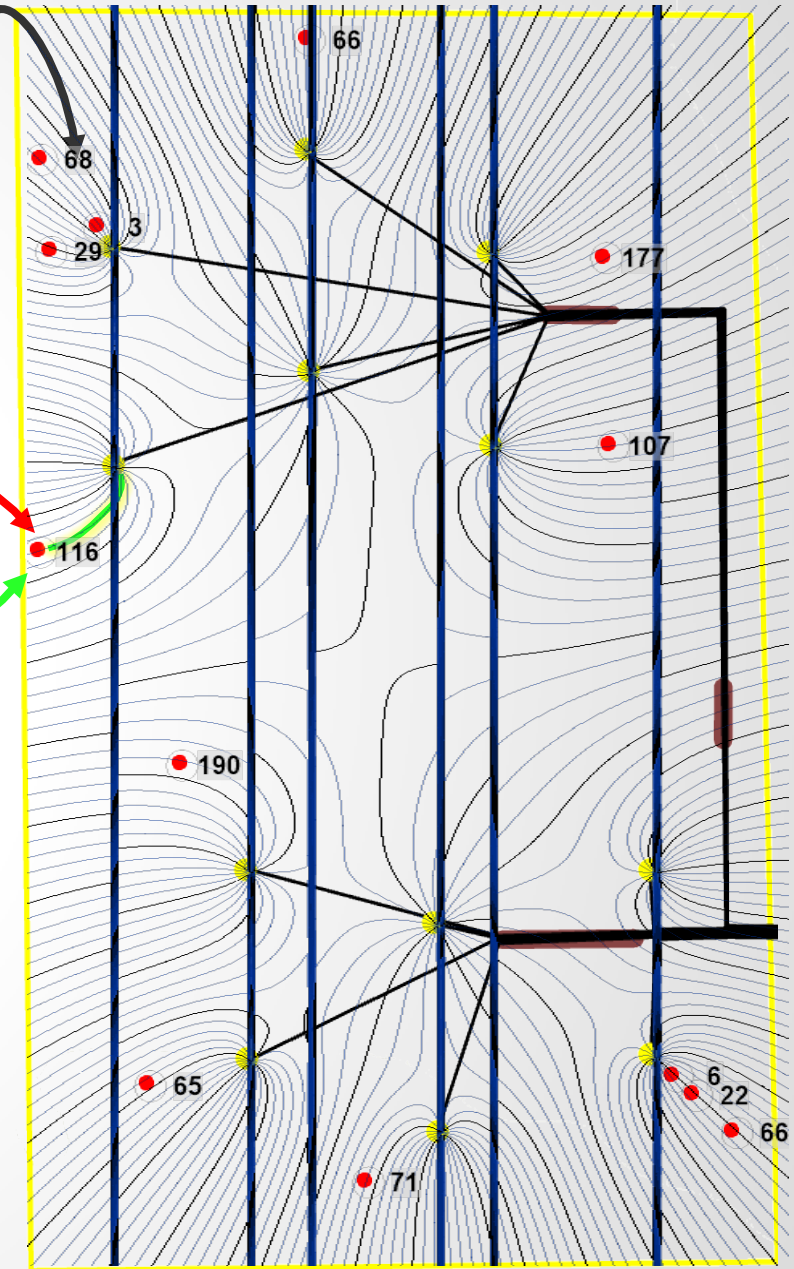
- Larger portion of aquifer represented
- Vapor Monitoring points were placed on the edge of remedial area to support evaluation of larger extent of remediation
- Earlier pilot started with vapor points interior and had to expand outward during the test
- **Average degradation across 6 acres → 23K gal/yr**

Actual oxygen volume injected should have degraded 21K gal/yr

Travel Time in Hours
for 54 SCFM distributed
across all wells

Formation Area
Represented by
Respiration Test

Formation Area
Represented by
Flow Model



Where to Go From Here

Both Respiration methods result in same conclusions in terms of rates as well as optimization recommendations

AEM flow models could optimize traditional respiration testing method (Leeson and Hincsee, 1995)

- Similar data collection – Smaller events but more frequent, more confidence
- Automated calculations
- No need to shut system down
- Provides an advective regime which could help sites that can not achieve diffusion during shutdown for standard testing method
- Standard respiration test or helium injection could help calibrate porosity or thickness in the AEM
- Even if absolute values are off, the time trends of soil gas levels at individual location will help estimate trends in rates

Outcome depends on monitoring network design and ability to model flow regime

AEM has potential to be applied to unconfined vadose zones with constant head leaky layer elements

Same method has been applied to carbon dioxide and methane readings in wells

- Methane - represents NSZD rate in vadose zone or perhaps from below the water-table
- Carbon Dioxide
 - Good because CO₂ is produced from organic reactions and isn't produced when inorganics are oxidized such as iron sulfides
 - Caution as CO₂ can be buffered by carbonates or calcium oxides

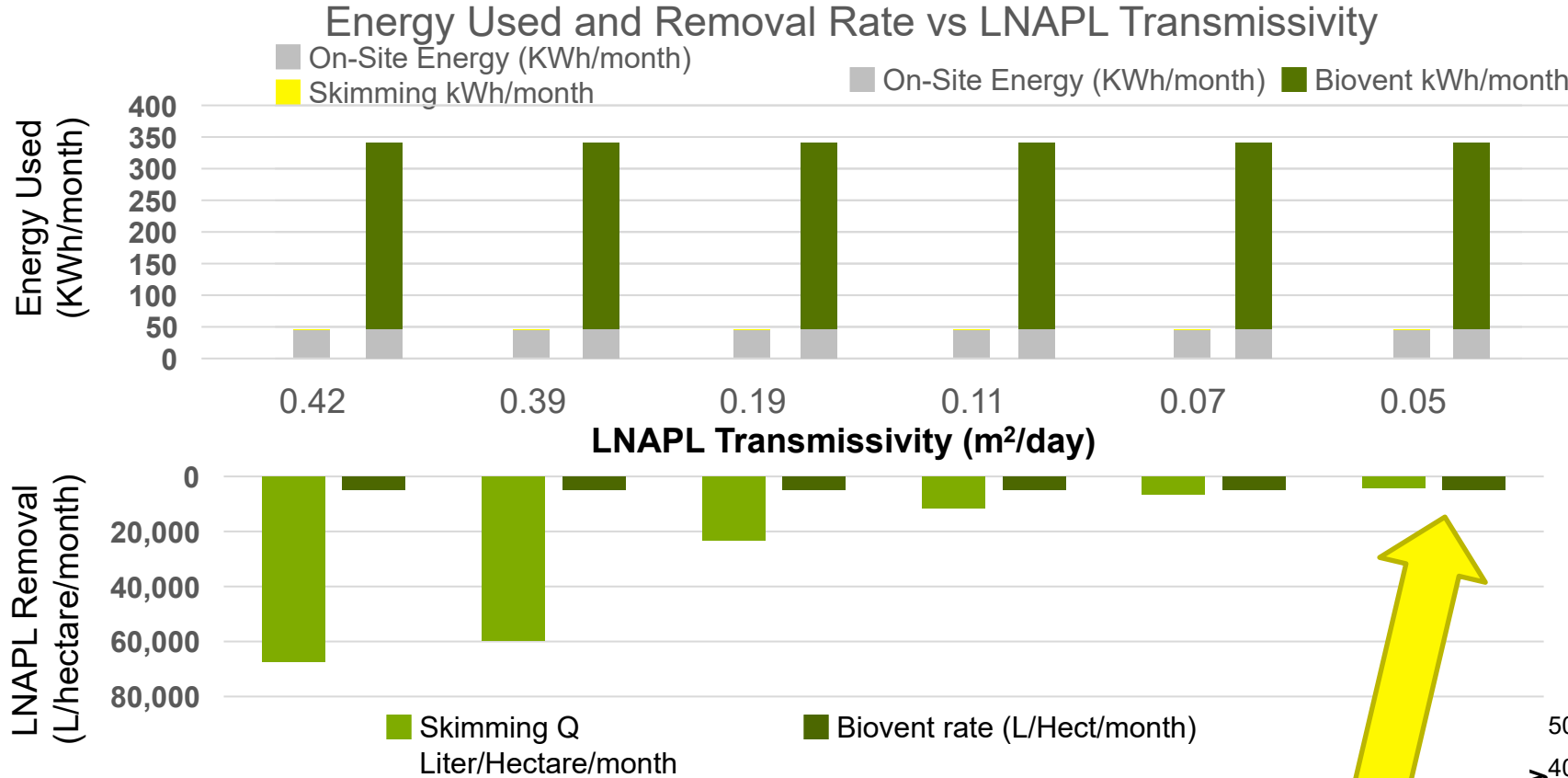
References

Leeson and Hinchee, *Bioventing Principles and Practice*, United States Environmental Protection Agency, EPA/540/R-95/534a, 1995.

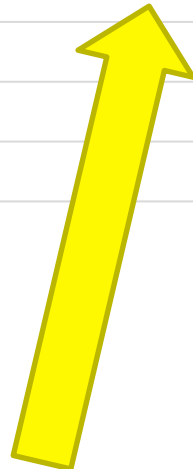
Strack, O.D.L., *Groundwater Mechanics*, Prentice Hall Englewood Cliffs, NJ 07632, 1989

Extras

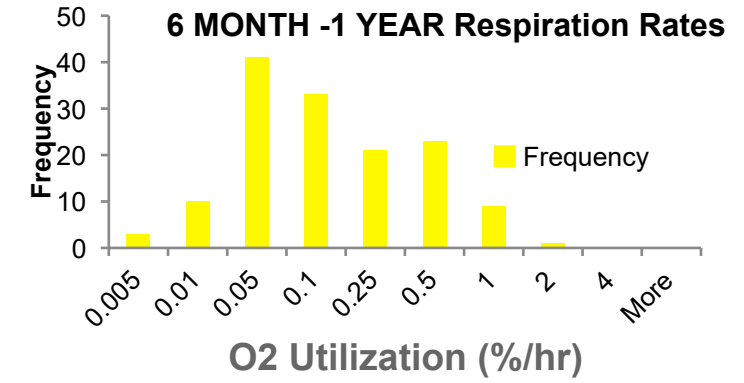
Energy Used Evaluation For a 3 m/day Sand



- Air – 50*Less viscous than water (Higher conductivity in soil than water)
- 2,000L air to treat 1L of LNAPL
- Bioventing Air Injection Rate 40 SCFM/ hectare is equivalent to
 - ~0.05%O₂/hr respiration or;
 - 4950 L/hectare/yr
- Actual biodegradation rate could be 10X higher
- Less Permeable Soils Proportionally more Energy, Higher Permeability Soils Proportionally less energy for Bioventing



Skimming 14% Energy & Equivalent Recovery rate



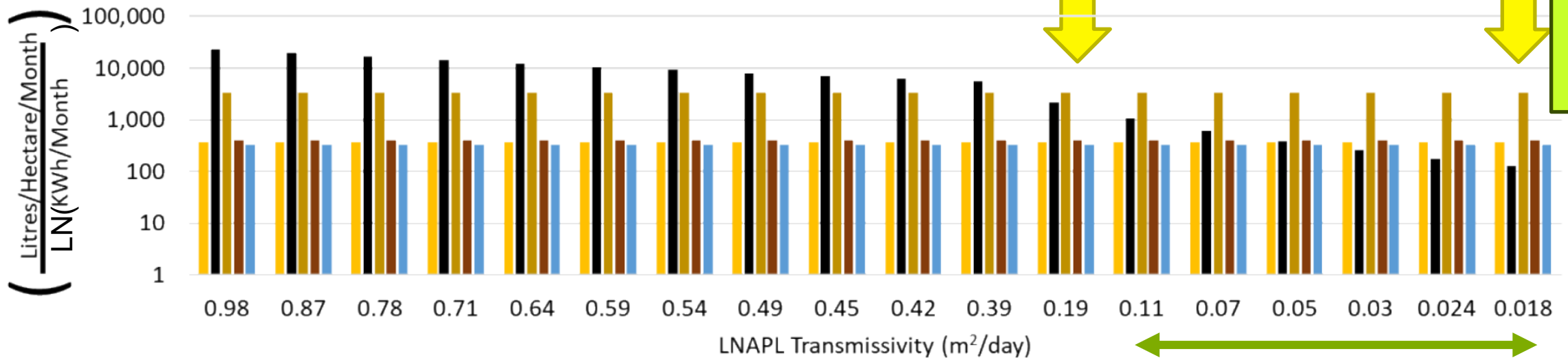
Revised Metric with LN(Energy)



LNAL Recovery (Skimming)
Recovery Rate/Energy vs LNAPL Transmissivity

Biovent

NSZD Sparg e?



- Balance Metric NSZD
- Balance Metric Skimming
- Balance Metric Biovent - 0.5 %O₂/hr
- Balance Metric Biovent - 0.05 %O₂/hr
- Balance Metric Sparge

Sparging likely requires an alternate driver to mass removal for implementation